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# THE STOCHASTIC MODELLING AND RELIABILITY ANALYSIS OF A BEER BOTTLE FILLING PLANT IN AN INDUSTRY

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## ABSTRACT

A model of Beer Bottle Filling Plant is developed for its stochastic analysis by personally visiting factory situated at District Samba in State Jammu and Kashmir. The said filling plant consists of five units- Conveyer belt, Filler, Crowner, Pasteurizer and Labeling Machine. Conveyer Belt is in series with other four units. The other four units are in parallel form but Filler machine is unified with crowner machine such that if any one of the two units fail, the other are kept in standby mode. After random period of time, if repair of failed unit is not completed then other units are kept in standby mode. If one unit is already in repair and within this period some other unit also fails then the whole system is put under emergency repair in order to make system ready as early as possible. A single repair facility is always available with the system to repair a failed unit. All the failure time distributions are taken to be negative exponential and all the repair time distributions are taken as arbitrary.

## KEYWORDS

Reliability; Availability; Busy period; Expected number of Repairs; Profit Analysis; Graphical study of Model.

## 1. INTRODUCTION

Although a lot of work has been done in the field of reliability by formulating and analyzing various kinds of system models, but most of the work done is of hypothetical nature and is not of much practical utility. Singh, S.K. and G. Nair Sheeba [10] have analyzed stone crushing system used in iron ore mines. Kumar Pawan and Bharti Ankush [7] formulated and carried out reliability analysis of a battery production system in an industry. Gupta and Ramkishan [5] developed a model pertaining to electric power, inverter and generator and obtained various reliability measures. Gupta and Shivakar [6] carried out the analysis w.r.t. reliability characteristics of a cloth manufacturing system model. Gupta, Varshney and Sharma [3] obtained various measures of system effectiveness of a milk powder making system in dairy plant. Besides these Malik et. al. [8,9] formulated and analyzed a system model of concrete mixture plant with preventive maintenance and also carried out a study on the comparison of various reliability characteristics of Haryana textile units. Sharma and Panigrahi [12], Arora and Kumar [1] have also studied the industrial system models with real existing situations.

For the purpose of analyzing real existing system, a model of beer bottle filling plant is developed for its stochastic analysis by personally visiting the plant situated in Samba district of state J&K.

The given plant consists of five units of varying nature. The working of different units of the system is described as follows:

- CONVEYOR BELT:** The conveyor belt conveys bottles from one machine to another one.
- FILLER MACHINE:** The bottle is pressed against the filling head and the evacuation valve of filler machine is opened, thereafter bottle is evacuated. By additional opening of preparatory valve, CO<sub>2</sub> is fed into the bottle and through second evacuation, the residual air is removed from it. Thereafter the beer valve opens and the beer flows along the wall into the bottle. The filling end is reached when the beer has reached the return pipe then beer and return valves are closed. The filler pressure, temperature and dosage of beverage quantity are preset.
- CROWNER MACHINE:** After filling, the bottles are directed to the crowner machine. It is necessary to fill the bottles as quickly as possible and subsequently to seal them immediately. For this purpose, the filler machine is unified with crowner machine. In the crowner machine, the first closure phase crown corks on bottles and second closure phase puts pressure on bottle to close rings of crown corks. Then the bottles are put on a slat conveyor belt.
- PASTEURIZER:** From slat conveyor belt, the bottles enter in pasteurizer. Pasteurizer is the best method of securing the shelf life of beverage. During pasteurization, the bottles, standing on conveyor belt, are fed slowly through the tunnel pasteurizer and at the same time warmed up by spraying on them warm and hot water of fixed temperature, then pasteurized and subsequently cooled down again.
- LABELING MACHINE:** After the pasteurization, the bottles are put forward to labeling machine by slat conveyor belt. The labeling machine has gluing pallets which roll against the gluing roller and are equipped there with a thin adhesive film. Each gluing pallet rolls against the label magazine and picks up one label at a time. The label is caught by gripping finger at the gripped cylinder and the glued backside facing outwards is transferred onto the bottle and brushed on.

Using the regenerative point technique the following important reliability characteristics of interest are obtained:

- Transition probabilities and mean sojourn times.
- Reliability and Mean time to system failure.
- Point wise and steady-state availabilities of the system.
- Expected up time of the system.
- Expected busy time of the repairman during  $(0, t]$  and in the steady-state.
- Expected number of repairs by repairman during  $(0, t]$  and in the steady-state.
- Net expected profit incurred by the system during  $(0, t]$  and in the steady-state.

## 2. SYSTEM DESCRIPTION AND ASSUMPTIONS

- The system consists of five non-identical units. Initially all the units are operative.
- Conveyer Belt is arranged in series with other four units. The other four units are in parallel form but Filler machine is unified with crowner machine such that if any one of the two units fails, the other are kept in standby mode.
- If repair of failed unit is not completed then after random period of time other units are kept in standby mode.



- d) If one unit is already in repair and the other unit also fails within this period then the whole system is put under emergency repair in order to make system ready as early as possible.
- e) A single repair facility is always available with the system to repair a failed unit.
- f) A repaired unit is as good as new and is immediately reconnected to the system.
- g) All the failure time distributions are taken to be negative exponential.
- h) All the repair time distributions are taken as arbitrary.

### 3. NOTATIONS AND SYMBOLS

- $\lambda$  : Constant failure rate of another unit when one unit is already failed.
- $\lambda_1$  : Constant rate with which the system is in down state.
- $\alpha$  : Failure rate of unit **CB** (conveyer belt).
- $G(\cdot)$  : C.d.f. of emergency repair time.
- $G_1(\cdot)$  : C.d.f. of repair time of unit **CB**.
- $\beta_i$  ( $i = 1, 2$ ) : Failure rate of unit **F/C** respectively.
- $\gamma_i$  ( $i = 1, 2$ ) : Failure rate of unit **P/L** respectively.
- $H_i(\cdot)$  ( $i = 1, 2$ ) : C.d.f. of repair time of unit **F/C** respectively.
- $F_i(\cdot)$  ( $i = 1, 2$ ) : C.d.f. of repair time of unit **P/L** respectively.
- $m_i$  ( $i = 1, 2$ ) : mean repair time of unit **F/C** respectively.
- $n_i$  ( $i = 1, 2$ ) : mean repair time of unit **P/L** respectively.
- $k_i/k$  : mean repair time of **CB**/ emergency repair.

#### Symbols for the states of the system

- $CB_0/CB_s/CB_r$  : Conveyer belt is operative/ in standby mode/ under repair.
- $F_0/F_s/F_r$  : Filler machine is operative/ in standby mode/ under repair.
- $C_0/C_s/C_r$  : Crouner machine is operative/ in standby mode/ under repair.
- $P_0/P_s/P_r$  : Pasteurizer is operative/ in standby mode/ under repair.
- $L_0/L_s/L_r$  : Labeling machine is operative/ in standby mode/ under repair.

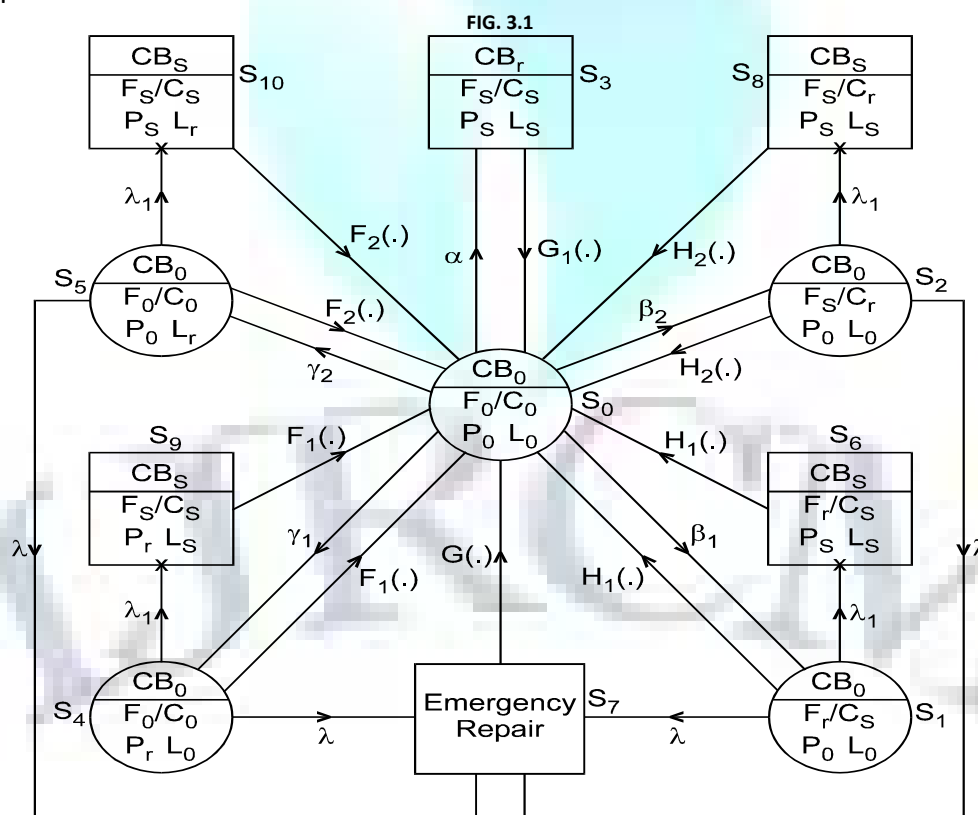
**Emergency Repair** : system is put under emergency repair, when any two units of the system are failed.

With the help of the above symbols, the possible states of the system are:

- $S_0 = [CB_0, F_0, C_0, P_0, L_0]$ ,  $S_1 = [CB_0, F_r, C_s, P_0, L_0]$
- $S_2 = [CB_0, F_s, C_r, P_0, L_0]$ ,  $S_3 = [CB_r, F_s, C_s, P_s, L_s]$
- $S_4 = [CB_0, F_0, C_0, P_r, L_0]$ ,  $S_5 = [CB_0, F_0, C_0, P_0, L_r]$
- $S_6 = [CB_s, F_r, C_s, P_s, L_s]$ ,  $S_7 = [\text{Emergency repair}]$
- $S_8 = [CB_s, F_s, C_r, P_s, L_s]$ ,  $S_9 = [CB_s, F_s, C_s, P_r, L_s]$
- $S_{10} = [CB_s, F_s, C_s, P_s, L_r]$

The transition diagram along with all transitions is shown in Fig. 3.1.

#### TRANSITION DIAGRAM



### 4. TRANSITION PROBABILITIES AND SOJOURN TIMES

Let  $T_0 (\equiv 0)$ ,  $T_1, T_2, \dots$  denotes the regenerative epochs and  $X_n$  denotes the state visited at epoch  $T_n$  i.e just after the transition at  $T_n$ . Then  $\{X_n, T_n\}$  constitute a Markov-Renewal process with state space  $E$ , set of regenerative states and

$$Q_{ij}(t) = P[X_{n+1} = j, T_{n+1} - T_n \leq t | X_n = i]$$

is the semi Markov kernel over  $E$ .

(a) Thus steady state transition probabilities can be obtained as follows:

$$p_{ij} = \lim_{t \rightarrow \infty} Q_{ij}(t)$$

So that,

$$\begin{aligned} p_{01} &= \frac{\beta_1}{(\alpha + \beta_1 + \beta_2 + \gamma_1 + \gamma_2)} & p_{02} &= \frac{\beta_2}{(\alpha + \beta_1 + \beta_2 + \gamma_1 + \gamma_2)} \\ p_{03} &= \frac{\alpha}{(\alpha + \beta_1 + \beta_2 + \gamma_1 + \gamma_2)} & p_{04} &= \frac{\gamma_1}{(\alpha + \beta_1 + \beta_2 + \gamma_1 + \gamma_2)} \\ p_{05} &= \frac{\gamma_2}{(\alpha + \beta_1 + \beta_2 + \gamma_1 + \gamma_2)} & p_{10} &= \tilde{H}_1(\lambda + \lambda_1) \\ p_{10}^{(6)} &= \frac{\lambda_1}{(\lambda + \lambda_1)} [1 - \tilde{H}_1(\lambda + \lambda_1)] & p_{17} &= \frac{\lambda}{(\lambda + \lambda_1)} [1 - \tilde{H}_1(\lambda + \lambda_1)] \\ p_{20} &= \tilde{H}_2(\lambda + \lambda_1) & p_{20}^{(8)} &= \frac{\lambda_1}{(\lambda + \lambda_1)} [1 - \tilde{H}_2(\lambda + \lambda_1)] \\ p_{27} &= \frac{\lambda}{(\lambda + \lambda_1)} [1 - \tilde{H}_2(\lambda + \lambda_1)] & p_{40} &= \tilde{F}_1(\lambda + \lambda_1) \\ p_{40}^{(9)} &= \frac{\lambda_1}{(\lambda + \lambda_1)} [1 - \tilde{F}_1(\lambda + \lambda_1)] & p_{47} &= \frac{\lambda}{(\lambda + \lambda_1)} [1 - \tilde{F}_1(\lambda + \lambda_1)] \\ p_{50} &= \tilde{F}_2(\lambda + \lambda_1) & p_{50}^{(10)} &= \frac{\lambda_1}{(\lambda + \lambda_1)} [1 - \tilde{F}_2(\lambda + \lambda_1)] \\ p_{57} &= \frac{\lambda}{(\lambda + \lambda_1)} [1 - \tilde{F}_2(\lambda + \lambda_1)] \end{aligned} \quad (1-17)$$

It can be easily seen that the following results hold good:

$$\begin{aligned} p_{01} + p_{02} + p_{03} + p_{04} + p_{05} &= 1 & p_{10} + p_{10}^{(6)} + p_{17} &= 1 \\ p_{20} + p_{20}^{(8)} + p_{27} &= 1 & p_{40} + p_{40}^{(9)} + p_{47} &= 1 \\ p_{50} + p_{50}^{(10)} + p_{57} &= 1 \\ p_{30} = p_{60} = p_{70} = p_{80} = p_{90} = p_{10,0} &= 1 \end{aligned} \quad (18-23)$$

(b) Mean sojourn times:

The mean sojourn time in state  $S_i$  denoted by  $\Psi_i$  is defined as the expected time taken by the system in state  $S_i$  before transiting to any other state. To obtain mean sojourn time  $\Psi_i$  in state  $S_i$ , we observe that as long as the system is in state  $S_i$ , there is no transition from  $S_i$  to any other state. If  $T_i$  denotes the sojourn time in state  $S_i$  then mean sojourn time  $\Psi_i$  in state  $S_i$  is:

$$\Psi_i = E[T_i] = \int P(T_i > t) dt \quad (24)$$

Thus

$$\begin{aligned} \Psi_0 &= \int e^{-(\alpha + \beta_1 + \beta_2 + \gamma_1 + \gamma_2)t} dt = \frac{1}{(\alpha + \beta_1 + \beta_2 + \gamma_1 + \gamma_2)} \\ \Psi_1 &= \int e^{-(\lambda + \lambda_1)t} \tilde{H}_1(t) dt = \frac{1}{(\lambda + \lambda_1)} [1 - \tilde{H}_1(\lambda + \lambda_1)] \\ \Psi_2 &= \int e^{-(\lambda + \lambda_1)t} \tilde{H}_2(t) dt = \frac{1}{(\lambda + \lambda_1)} [1 - \tilde{H}_2(\lambda + \lambda_1)] \\ \Psi_3 &= \int \tilde{G}_1(t) dt = k_1 \\ \Psi_4 &= \int e^{-(\lambda + \lambda_1)t} \tilde{F}_1(t) dt = \frac{1}{(\lambda + \lambda_1)} [1 - \tilde{F}_1(\lambda + \lambda_1)] \\ \Psi_5 &= \int e^{-(\lambda + \lambda_1)t} \tilde{F}_2(t) dt = \frac{1}{(\lambda + \lambda_1)} [1 - \tilde{F}_2(\lambda + \lambda_1)] \\ \Psi_6 &= \int \tilde{H}_1(t) dt = m_1 \\ \Psi_7 &= \int \tilde{G}(t) dt = k \\ \Psi_8 &= \int \tilde{H}_2(t) dt = m_2 \\ \Psi_9 &= \int \tilde{F}_1(t) dt = n_1 \\ \Psi_{10} &= \int \tilde{F}_2(t) dt = n_2 \end{aligned} \quad (25-35)$$

## 5. ANALYSIS OF RELIABILITY AND MTSF

Let the random variable  $T_i$  be the time to system failure when system starts up from state  $S_i \in E_i$ , the the reliability of the system is given by

$$R_i(t) = P[T_i > t]$$

To determine,  $R_i(t)$  we regard the failed states ( $S_3, S_6, S_7, S_8, S_9, S_{10}$ ) of the system as absorbing. Using the simple probabilistic arguments, one can easily develop the recurrence relations among  $R_i(t)$ ;  $i = 0, 1, 2, 4, 5$ . Taking the Laplace Transforms of these relations and simplifying the resulting set of algebraic equations for,  $R_0^*(s)$  after omitting the arguments 's' for brevity, we get

$$R_0^*(s) = N_1(s)/D_1(s) \quad (36)$$

where,

$$N_1(s) = (Z_0^* + q_{01}^* Z_1^* + q_{02}^* Z_2^* + q_{04}^* Z_4^* + q_{05}^* Z_5^*)$$

and

$$D_1(s) = [1 - (q_{01}^* q_{10}^* + q_{02}^* q_{20}^* + q_{04}^* q_{40}^* + q_{05}^* q_{50}^*)]$$

where,  $Z_0^*, Z_1^*, Z_2^*, Z_4^*, Z_5^*$  are the Laplace transforms of

$$Z_0(t) = e^{-(\alpha + \beta_1 + \beta_2 + \gamma_1 + \gamma_2)t}, \quad Z_1(t) = e^{-(\lambda + \lambda_1)t} \tilde{H}_1(t), \quad Z_2(t) = e^{-(\lambda + \lambda_1)t} \tilde{H}_2(t)$$

$$Z_4(t) = e^{-(\lambda + \lambda_1)t} \tilde{F}_1(t), \quad Z_5(t) = e^{-(\lambda + \lambda_1)t} \tilde{F}_2(t)$$

Taking inverse Laplace Transform of (36), we get reliability of the system.

To get MTSF, we use the well-known formula

$$E(T_0) = \int R_0(t) dt = \lim_{s \rightarrow 0} R_0^*(s) = N_1(0)/D_1(0) \quad (37)$$

where,

$$N_1(0) = (\Psi_0 + p_{01}\Psi_1 + p_{02}\Psi_2 + p_{04}\Psi_4 + p_{05}\Psi_5)$$

and

$$D_1(0) = [1 - (p_{01}p_{10} + p_{02}p_{20} + p_{04}p_{40} + p_{05}p_{50})]$$

Here we use the relations  $q_{ij}^*(0) = p_{ij}$  and  $\lim_{s \rightarrow 0} Z_i^*(s) = \int Z_i(t) dt = \Psi_i$ .

## 6. AVAILABILITY ANALYSIS

Define  $A_i(t)$  as the probability that the system is up at epoch 't' when it initially started from regenerative state  $S_i \in E_i$ . Using the definition of  $A_i(t)$  and probabilistic concepts, the recurrence relations among  $A_i(t)$  where  $i = 0, 1, 2, 3, 4, 5, 7$  can easily be developed.

Using the technique of L.T., the value of  $A_0(t)$  in terms of its L.T. is as follows:

$$A_0^*(s) = N_2(s)/D_2(s) \quad (38)$$

where,

$$N_2(s) = (Z_0^* + q_{01}^* Z_1^* + q_{02}^* Z_2^* + q_{04}^* Z_4^* + q_{05}^* Z_5^*) \quad (39)$$

and

$$D_2(s) = 1 - [q_{01}^*(q_{10}^* + q_{10}^{(6)*} + q_{17}^*q_{70}^*) + q_{02}^*(q_{20}^* + q_{20}^{(8)*} + q_{27}^*q_{70}^*) + q_{03}^*q_{30}^* + q_{04}^*(q_{40}^* + q_{40}^{(9)*} + q_{47}^*q_{70}^*) + q_{05}^*(q_{50}^* + q_{50}^{(10)*} + q_{57}^*q_{70}^*)] \quad (40)$$

The steady state availability of the system, i.e. probability that in the long run the system will be up, is given by

$$A_0 = \lim_{t \rightarrow \infty} A_0(t) = \lim_{s \rightarrow 0} s A_0^*(s) = \lim_{s \rightarrow 0} \frac{s N_2(s)}{D_2(s)} = \lim_{s \rightarrow 0} N_2(s) \lim_{s \rightarrow 0} \frac{s}{D_2(s)}$$

As  $s \rightarrow 0$ , the above equation becomes indeterminate form.

Hence on using L'Hospital's rule,  $A_0$  becomes

$$A_0 = N_2(0)/D_2'(0) \quad (41)$$

where,

$$N_2(0) = (\Psi_0 + p_{01}\Psi_1 + p_{02}\Psi_2 + p_{04}\Psi_4 + p_{05}\Psi_5) \quad (42)$$

and

$$D_2'(0) = \Psi_0 + p_{01}\Psi_1 + p_{02}\Psi_2 + p_{03}k_1 + p_{04}\Psi_4 + p_{05}\Psi_5 + Ak \quad (43)$$

where,  $A = p_{01}p_{17} + p_{02}p_{27} + p_{04}p_{47} + p_{05}p_{57}$

The expected up time of the system during  $(0, t]$  is given by

$$\mu_{up}(t) = \int_0^t A_0(u) du$$

So that,

$$\mu_{up}^*(s) = A_0^*(s)/s. \quad (44)$$

## 7. BUSY PERIOD ANALYSIS

Define  $B_i(t)$  as the probability that the system having started from regenerative state  $S_i \in E$  at time  $t = 0$ , is under repair at time ' $t$ ' due to failure of the unit.

Using the definition of  $B_i(t)$  and probabilistic concepts, the recurrence relations among  $B_i(t)$  where  $i = 0, 1, 2, 3, 4, 5, 7$  can easily be developed.

Using the technique of L.T., the value of  $B_0(t)$  in terms of its L.T. is as follows:

$$B_0^*(s) = N_3(s)/D_2(s) \quad (45)$$

where,

$$N_3(s) = (q_{01}^*Z_1^* + q_{02}^*Z_2^* + q_{03}^*Z_3^* + q_{04}^*Z_4^* + q_{05}^*Z_5^*) + (q_{01}^*q_{17}^* + q_{02}^*q_{27}^* + q_{04}^*q_{47}^* + q_{05}^*q_{57}^*)Z_7^* \quad (46)$$

In steady state, the probability that the repairman will be busy is given by

$$B_0 = \lim_{t \rightarrow \infty} B_0(t) = \lim_{s \rightarrow 0} s B_0^*(s) = N_3(0)/D_2'(0) \quad (47)$$

also as  $s \rightarrow 0$ ,  $q_{ij}^*(s)/s = q_{ij}^*(0) = p_{ij}$  and  $\lim_{s \rightarrow 0} Z_i^*(s) = \int Z_i(t)dt = \Psi_i$

where,

$$N_3(0) = (p_{01}\Psi_1 + p_{02}\Psi_2 + p_{03}k_1 + p_{04}\Psi_4 + p_{05}\Psi_5) + (p_{01}p_{17} + p_{02}p_{27} + p_{04}p_{47} + p_{05}p_{57})k \quad (48)$$

The expected busy period of the repairman during  $(0, t]$  is given by

$$\mu_b(t) = \int_0^t B_0(u) du$$

So that,

$$\mu_b^*(s) = B_0^*(s)/s. \quad (49)$$

## 8. EXPECTED NUMBER OF REPAIRS

Let us define  $V_i(t)$  as the expected number of repairs of the failed units during the time interval  $(0, t]$  when the system initially starts from regenerative state  $S_i$ . Using the definition of  $V_i(t)$  and probabilistic concepts, the recurrence relations among  $V_i(t)$  where  $i = 0, 1, 2, 3, 4, 5, 7$  can easily be developed.

Using the technique of L.S.T., the solution for  $\tilde{V}_0(s)$  is given by

$$\tilde{V}_0(s) = N_4(s)/D_4(s) \quad (50)$$

where,

$$N_4(s) = \tilde{Q}_{01}(\tilde{Q}_{10} + \tilde{Q}_{10}^{(6)} + \tilde{Q}_{17}\tilde{Q}_{70}) + \tilde{Q}_{02}(\tilde{Q}_{20} + \tilde{Q}_{20}^{(8)} + \tilde{Q}_{27}\tilde{Q}_{70}) + \tilde{Q}_{03}\tilde{Q}_{30} + \tilde{Q}_{04}(\tilde{Q}_{40} + \tilde{Q}_{40}^{(9)} + \tilde{Q}_{47}\tilde{Q}_{70}) + \tilde{Q}_{05}(\tilde{Q}_{50} + \tilde{Q}_{50}^{(10)} + \tilde{Q}_{57}\tilde{Q}_{70}) \quad (51)$$

$D_4(s)$  can be written on replacing  $q_{ij}^*$  by  $\tilde{Q}_{ij}$  in  $D_2(s)$  given by (40)

In the steady state, the expected number of repairs per unit time is given by

$$V_0 = \lim_{t \rightarrow \infty} \left[ \frac{V_0(t)}{t} \right] = \lim_{s \rightarrow 0} s \tilde{V}_0(s) = N_4(0)/D_4'(0)$$

where,

$$N_4(0) = p_{01}(p_{10} + p_{10}^{(6)} + p_{17}p_{70}) + p_{02}(p_{20} + p_{20}^{(8)} + p_{27}p_{70}) + p_{03}p_{30} + p_{04}(p_{40} + p_{40}^{(9)} + p_{47}p_{70}) + p_{05}(p_{50} + p_{50}^{(10)} + p_{57}p_{70}) \quad (52)$$

## 9. PROFIT FUNCTION ANALYSIS

Two profit functions  $P_1(t)$  and  $P_2(t)$  can easily be obtained for the system model under study with the help of characteristics obtained earlier. The expected total profits incurred during  $(0, t]$  are:

$$P_1(t) = \text{Expected total revenue in } (0, t] - \text{Expected total expenditure in } (0, t] \\ = K_0\mu_{up}(t) - K_1\mu_b(t) \quad (53)$$

Similarly,

$$P_2(t) = K_0\mu_{up}(t) - K_2V_0(t) \quad (54)$$

where,

$K_0$  is revenue per unit up time.

$K_1$  is the cost per unit time for which repair man is busy in repair of the failed unit.

$K_2$  is per unit repair cost.

The expected total profits per unit time, in steady state, is

$$P_1 = \lim_{t \rightarrow \infty} [P_1(t)/t] = \lim_{s \rightarrow 0} s^2 P_1^*(s)$$

$$P_2 = \lim_{t \rightarrow \infty} [P_2(t)/t] = \lim_{s \rightarrow 0} s^2 P_2^*(s)$$

So that,

$$P_1 = K_0A_0 - K_1B_0 \quad (55)$$

and

$$P_2 = K_0A_0 - K_2V_0 \quad (56)$$

## 10. PARTICULAR CASE

If the repair time distributions are taken as negative exponential i.e.

$$G(t) = 1 - e^{-\eta t} \quad G_1(t) = 1 - e^{-\alpha_1 t} \\ H_i(t) = 1 - e^{-\theta_i t} \quad F_i(t) = 1 - e^{-\mu_i t} \quad \text{where, } (i = 1, 2)$$

Then the variations in transition probabilities and mean sojourn times are as follows:

$$\begin{aligned}
 p_{10} &= \frac{\theta_1}{(\lambda + \lambda_1 + \theta_1)} & p_{10}^{(6)} &= \frac{\lambda_1}{(\lambda + \lambda_1 + \theta_1)} & p_{17} &= \frac{\lambda}{(\lambda + \lambda_1 + \theta_1)} \\
 p_{20} &= \frac{\theta_2}{(\lambda + \lambda_1 + \theta_2)} & p_{20}^{(8)} &= \frac{\lambda_1}{(\lambda + \lambda_1 + \theta_2)} & p_{27} &= \frac{\lambda}{(\lambda + \lambda_1 + \theta_2)} \\
 p_{40} &= \frac{\mu_1}{(\lambda + \lambda_1 + \mu_1)} & p_{40}^{(9)} &= \frac{\lambda_1}{(\lambda + \lambda_1 + \mu_1)} & p_{17} &= \frac{\lambda}{(\lambda + \lambda_1 + \mu_1)} \\
 p_{50} &= \frac{\mu_2}{(\lambda + \lambda_1 + \mu_2)} & p_{40}^{(10)} &= \frac{\lambda_1}{(\lambda + \lambda_1 + \mu_2)} & p_{57} &= \frac{\lambda}{(\lambda + \lambda_1 + \mu_2)} \\
 \Psi_1 &= \frac{1}{(\lambda + \lambda_1 + \theta_1)} & \Psi_2 &= \frac{1}{(\lambda + \lambda_1 + \theta_2)} & \Psi_3 &= \frac{1}{\alpha_1} \\
 \Psi_4 &= \frac{1}{(\lambda + \lambda_1 + \mu_1)} & \Psi_5 &= \frac{1}{(\lambda + \lambda_1 + \mu_2)} & \Psi_6 &= \frac{1}{\theta_1} \\
 \Psi_7 &= \frac{1}{\eta} & \Psi_8 &= \frac{1}{\theta_2} & \Psi_9 &= \frac{1}{\mu_1} \\
 \Psi_{10} &= \frac{1}{\mu_2}
 \end{aligned}$$

## 11. GRAPHICAL STUDY OF THE SYSTEM MODEL

For more concrete study of system behavior, we plot MTSF and Profit functions with respect to  $\beta_1$  (failure rate of Filler machine) for different values of  $\theta_1$  (repair rate of Filler machine).

**Fig. 2** shows the variations in MTSF in respect of  $\beta_1$  for different values of  $\theta_1$  as 0.25, 0.50 and 0.75 while the other parameters are fixed as  $\lambda = 0.30$ ,  $\lambda_1 = 0.10$ ,  $\gamma_1 = 0.03$ ,  $\gamma_2 = 0.03$ ,  $\alpha = 0.20$ ,  $\alpha_1 = 0.30$ ,  $\beta_2 = 0.05$ ,  $\eta = 0.04$ ,  $\mu_1 = 0.02$ ,  $\mu_2 = 0.02$ ,  $\theta_2 = 0.05$ . It is observed from the graph that MTSF decreases with the increase in the failure parameter  $\beta_1$  and for higher values of  $\theta_1$ , the MTSF is higher i.e., the repair facility has a better understanding of failure phenomenon resulting in longer lifetime of the system.

**Fig. 3** represents the change in profit function  $P_1$  and  $P_2$  w.r.t.  $\beta_1$  for different values of  $\theta_1$  as 0.25, 0.50 and 0.75 while the other parameters are fixed as  $\lambda = 0.30$ ,  $\lambda_1 = 0.10$ ,  $\gamma_1 = 0.03$ ,  $\gamma_2 = 0.03$ ,  $\alpha = 0.20$ ,  $\alpha_1 = 0.30$ ,  $\beta_2 = 0.05$ ,  $\eta = 0.04$ ,  $\mu_1 = 0.02$ ,  $\mu_2 = 0.02$ ,  $\theta_2 = 0.05$ ,  $K_0 = 1000$ ,  $K_1 = 300$ ,  $K_2 = 250$ . From the graph it is seen that both profit functions decrease with the increase in failure rate  $\beta_1$  and increase with the increase in  $\theta_1$ . It is also observed that profit function  $P_2$  is always higher as compared to profit function  $P_1$  for fixed values of  $\beta_1$  and  $\theta_1$ . Thus the better understanding of failure phenomenon by the repairman results in better system performance.

## 12. CONCLUDING REMARKS

A model of Beer Bottle Filling Plant consisting of five units is developed and analyzed with respect to various reliability characteristics for its stochastic analysis by personally visiting the factory situated at District Samba in State Jammu and Kashmir. All the failure time distributions are taken to be negative exponential. All the repair time distributions are taken as arbitrary. The graphical study of some of the reliability characteristics has also been carried out.

FIG. 2

Behaviour of MTSF w.r.t.  $\beta_1$  for different values of  $\theta_1$

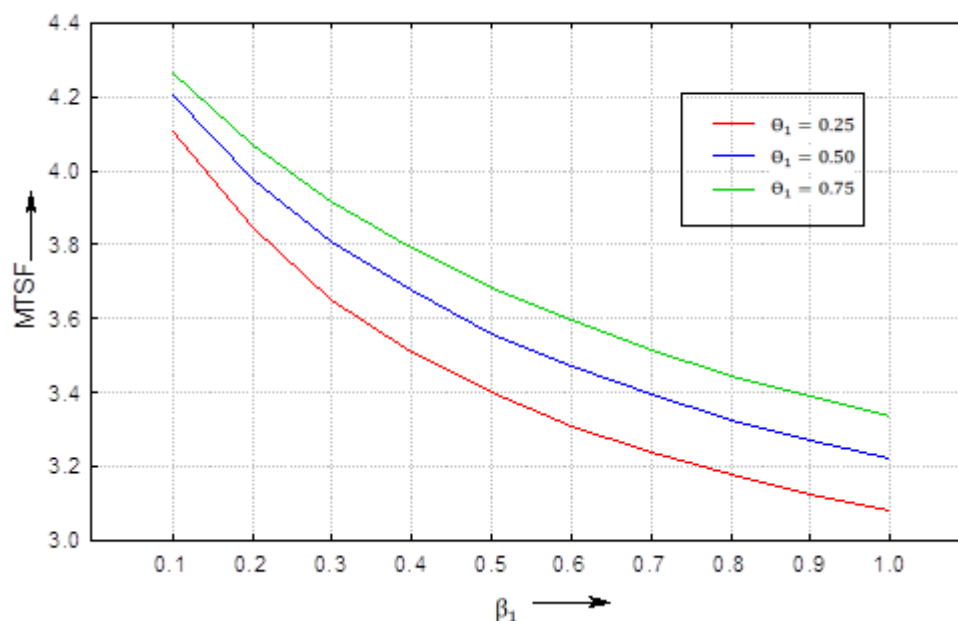
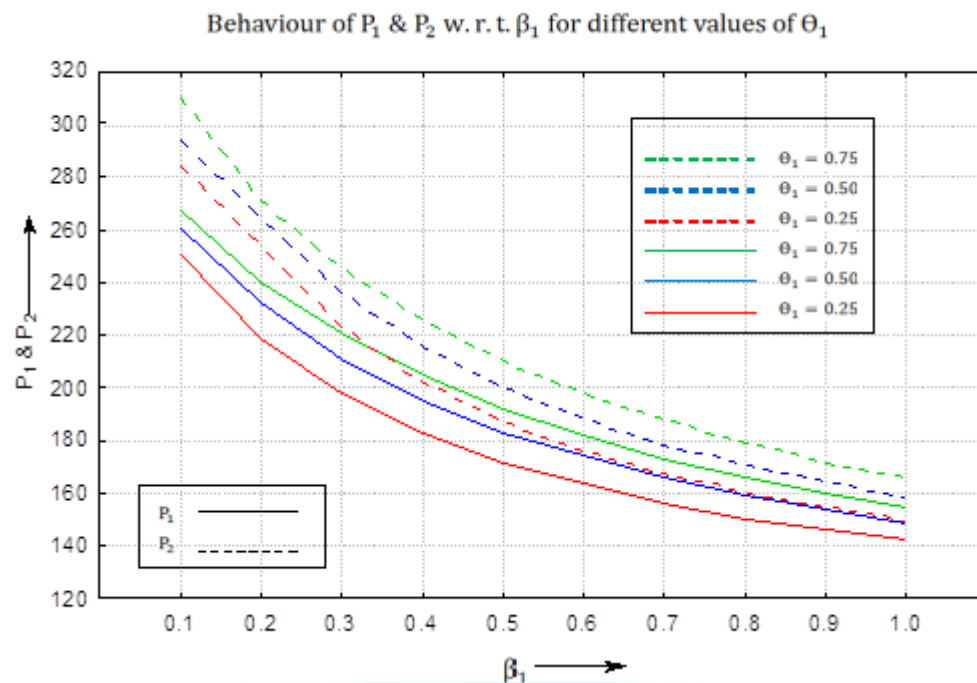


FIG. 3



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